

DE LA RECHERCHE À L'INDUSTRIE



# Study of a collocated Lagrange-Remap scheme for multimaterial flows adapted to HPC

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- 1 Collocated Lagrange-Remap scheme features
- 2 Collocated Lagrange scheme and entropy dissipation
- 3 Collocated Remap scheme and total energy

- The methods presented here are developed in the SHY code platform (Peybernes, Poncet, Motte, Rivoire), dedicated to research in HPC and numerics.
- The goal is to propose a **multimaterial Eulerian scheme** for the next generation of HPC hydrocodes:
  - ① Meshes will be refined: the scheme should be robust, second order in time and space and entropic at first order. If the scheme is conservative, it converges to the right solution.  
→ *Collocated Lagrange+Remap scheme*
  - ② Code scalability: the number of MPI parallel synchronisations should be limited and remap should be generic to allow OpenMP parallel loops and vectorization.  
→ *Direct multidirectional remap scheme*
- This study is restricted to 2D Cartesian orthogonal meshes and multimaterial flows with two materials (sharp interface).

Collocated Lagrangian schemes EUCCLHYD (P.-H. Maire et al, 2007) or GLACE (Després et al, 2005) solve this conservative system:

$$\left\{ \begin{array}{l} \frac{d}{dt} \int_{\Omega(t)} 1 dV \\ \frac{d\vec{x}(t)}{dt} \\ \frac{d}{dt} \int_{\Omega(t)} \rho(x, t) dV \\ \frac{d}{dt} \int_{\Omega(t)} \rho(x, t) \vec{u}(x, t) dV \\ \frac{d}{dt} \int_{\Omega(t)} \rho(x, t) E(x, t) dV \\ P(x, t) \end{array} \right. \begin{array}{l} = \int_{\Omega(t)} (\vec{\nabla} \cdot \vec{u})(x, t) dV \\ = \vec{u}(x, t) \\ = 0 \\ = - \int_{\Omega(t)} \vec{\nabla} P(x, t) dV \\ = - \int_{\Omega(t)} \vec{\nabla} \cdot (P(x, t) \vec{u})(x, t) dV \\ = P(\rho(x, t), e(x, t)) \end{array}$$

with  $\rho$  the density,  $P$  the pressure,  $E$  the specific total energy and  $\vec{u}$  the velocity on volume  $\Omega(t)$ .

## Multimaterial collocated Lagrange scheme steps:

S. Galera, P.-H. Maire, J. Breil. A two-dimensional unstructured cell-centered multimaterial ALE scheme using VOF interface reconstruction, *J. Comput. Phys.*, 229 (2010), 5755-5787.

1) **Acoustic Godunov Riemann problems at nodes** to obtain node velocities and pressures at half edges with constraints:

- volume and total energy conservation,
- entropy dissipation (first order).

2) Fluxes are computed with node velocities and half edges pressures, and variables  $(\vec{x}, V, \vec{u}, E)$  are updated.

3) In mixed cell  $i$  with materials  $\alpha$ :

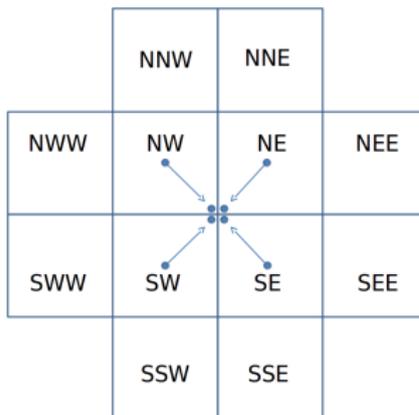
- velocity is the same for all materials,
- materials densities evolve considering iso-deformation,
- mixture pressure is materials pressures volume averaged,
- specific entropy dissipation rate is the same for all materials:

$$m_{\alpha} d_t e_{\alpha} + f_{\alpha} p_{\alpha} d_t Vol_i = m_{\alpha} (T d_t s)_i$$

# Collocated Lagrange scheme second order

- Second order in time with predictor-corrector integration.
- Second order in space for node velocities and pressures at half edges, by MUSCL reconstruction at nodes of cell centered variable  $P = (u, v, p)$ . For instance for SW:

$$P_{SW}^{order2} = P_{SW} + \frac{\varphi(\theta_{SW}^x)}{2}(P_{SW} - P_{SWW}) + \frac{\varphi(\theta_{SW}^y)}{2}(P_{SW} - P_{SSW})$$



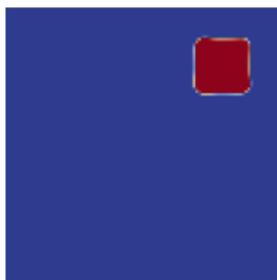
# Lagrange Wilkins + Remap: Alternate Directions vs Direct Remap

*Work with Bastien Chaudet, Master degree training 2014*

- Build a Direct remap using the same tools as the ADI remap
- Naive Direct FV remap not very accurate for multimaterial flows → **Direct remap with corner fluxes**
- “Alternate directions” does a good job in many situations.
- Direct remap with corner fluxes is a more complex algorithm, but it could worth when dealing with many cores (scalability).



Direct

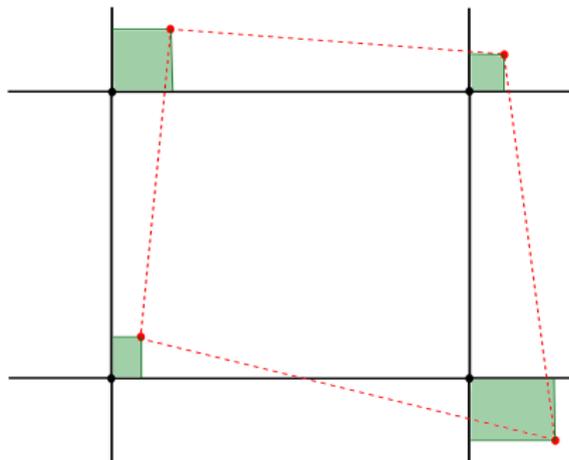


Alternate Directions

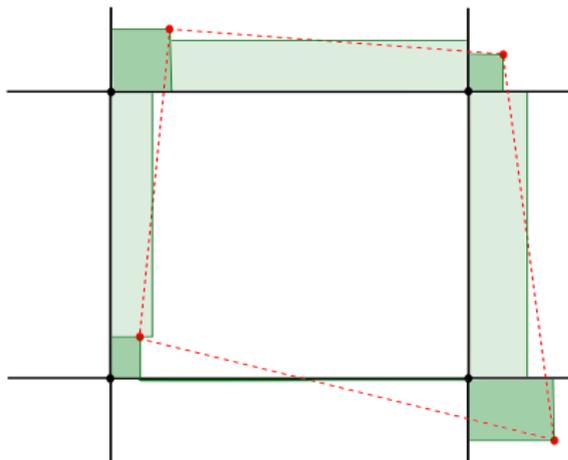


Direct Corner Fluxes

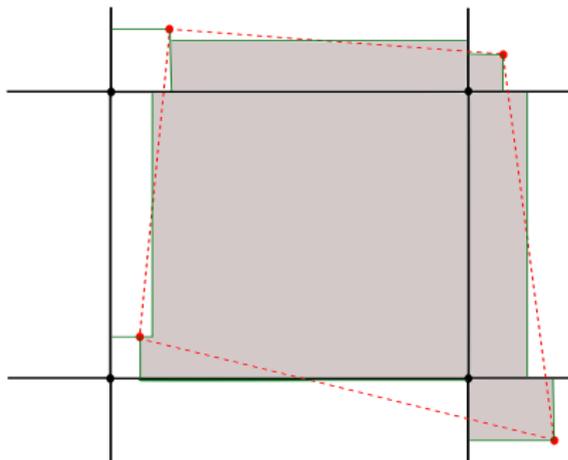
- Lagrangian displacement along all directions,
- Face fluxes, Corner fluxes.



- Lagrangian displacement along all directions,
- Face fluxes, Corner fluxes.



- Lagrangian displacement along all directions,
- Face fluxes, Corner fluxes.



# Direct Remap with Corner Fluxes

- Computation of multimaterial faces  $dVol_{\alpha f}$  and corners  $dVol_{\alpha c}$  volume fluxes,
- Interface positioning with volume fractions (Youngs) and rectangular approximation of the lagrangian cell.

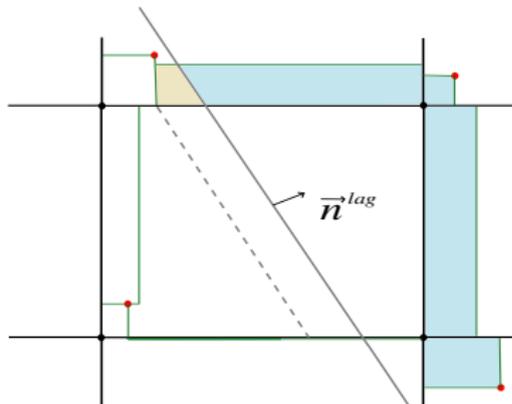


Figure : Intersection between the interface and faces and corners volume fluxes.

# Results Wilkins+Remap AD vs Direct with Corner Fluxes

- Interaction between a shock in air and a bubble of Helium. Mesh  $1000 \times 90$ , domain  $[0, 1000] \times [0, 9]$  cm.

Initial state	Left air state (shock)	Right air state	Bubble
Density $\rho$ ( $\text{kg.m}^3$ )	1.376363	1	0.18187
Velocity $\mathbf{u.e}_x$ ( $\text{m.s}^{-1}$ )	124.824	0	0
Pressure $p$ (Pa)	$1.5698 \cdot 10^5$	$10^5$	$10^5$
Gamma $\gamma$	1.4	1.4	1.66

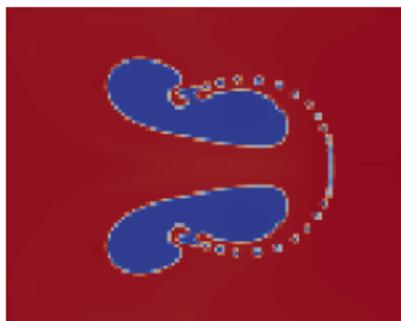
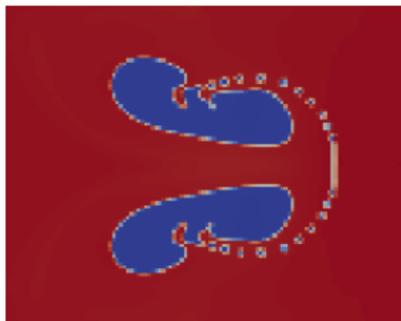


Figure : Zoom, density at final state,  $t = 1$  ms. ADI left, DirectCF right.

- Impact droplet on thin film: Impact of a water drop into air on a water wall. Mesh  $320 \times 160$ , domain  $[0, 10] \times [0, 5]$  cm. Multimaterial, air Perfect Gas, and water Stiffened Gas.

Initial state	Air	Wall	Drop
Density $\rho$ ( $\text{kg.m}^3$ )	1.29	1000	1000
Velocity $\mathbf{u.e}_x$ ( $\text{m.s}^{-1}$ )	-1000	0	-1000
Pressure $p$ (Pa)	$10^5$	$10^5$	$10^5$
Gamma $\gamma$	1.4	7	7
Pi $\pi$ (Pa)	0	$2.1 \cdot 10^9$	$2.1 \cdot 10^9$

# Results Wilkins+Remap AD vs Direct with Corner Fluxes

- Impact droplet on thin film: Impact of a water drop into air on a water wall. Mesh  $320 \times 160$ , domain  $[0, 10] \times [0, 5]$  cm.

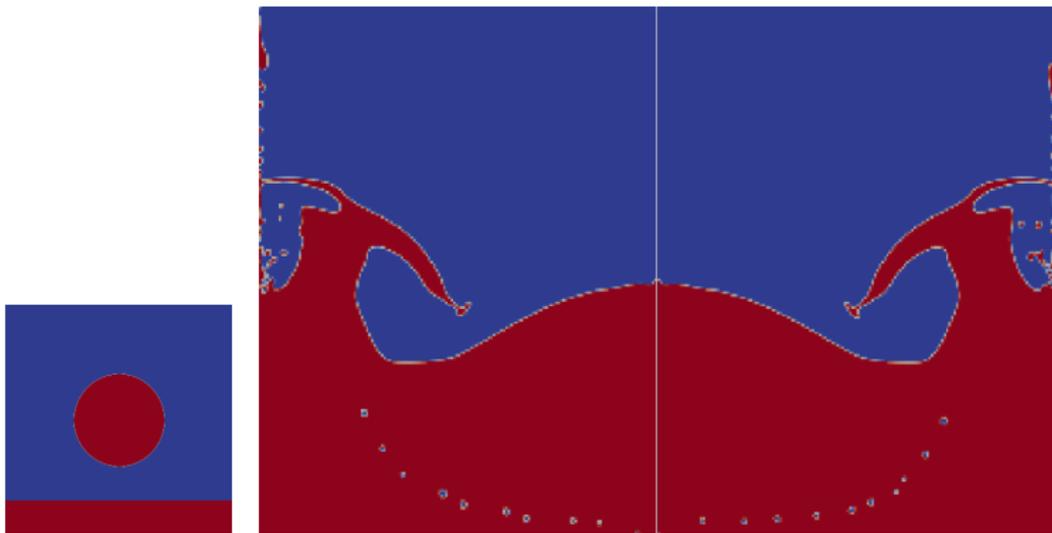


Figure : Volume fraction at initial state,  $t = 0$ s and  $t = 6$ s. ADI left, DirectCF right.

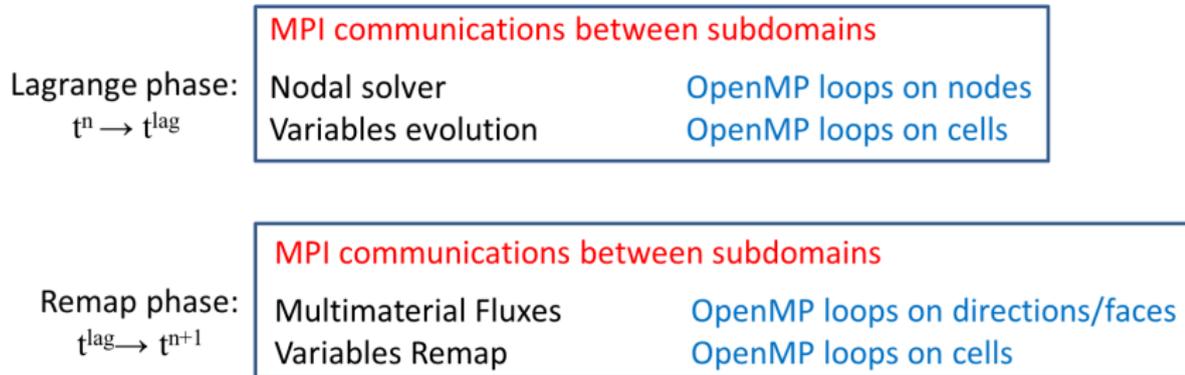


Figure : Sketch of the hybrid parallelization MPI-OpenMP.

→ Good scheme properties (numerics, HPC),

but entropy dissipation: can we diminish it ?

**FRAMEWORK:** the time derivative is considered at the discrete level, whatever the time integration scheme:

$$d_t A = \frac{A^{n+1} - A^n}{\Delta t}$$

For a cell  $i$ , EUCCLHYD scheme writes:

$$\begin{aligned}
 m_i d_t(1/\rho_i) &= [\nabla \cdot u]_i &= \int_{\Omega_i} \nabla \cdot u &= \sum_f A_f (u_f \cdot n_f) \\
 m_i d_t(u_i) &= -[\nabla p]_i &= \int_{\Omega_i} -\nabla p &= -\sum_f A_f p_f n_f \\
 m_i d_t(E_i) &= -[\nabla \cdot (p u)]_i &= \int_{\Omega_i} -\nabla \cdot (p u) &= -\sum_f A_f p_f (u_f \cdot n_f)
 \end{aligned} \tag{1}$$

Flux terms  $[\nabla \cdot u]_i$ ,  $[\nabla p]_i$ ,  $[\nabla \cdot (p u)]_i$  computation is detailed in EUCCLHYD literature.

In 1D,  $Vol_i = 1 \cdot \Delta x_i$  and EUCCLHYD is the Godunov acoustic scheme:

$$p_{i+1/2} = \bar{p}_{i+1/2} - \frac{\bar{\alpha}_{i+1/2}}{2}(u_{i+1} - u_i) \quad (2)$$

$$\rho_i d_t(u_i) = - \frac{\bar{p}_{i+1/2} - \bar{p}_{i-1/2}}{\Delta x_i} + \frac{\bar{\alpha}_{i+1/2}(u_{i+1} - u_i) - \bar{\alpha}_{i-1/2}(u_i - u_{i-1})}{2\Delta x_i} \quad (3)$$

# -  $\partial_x(p + q)$

with an equivalent linear artificial viscosity  $q = \frac{1}{2}\rho c \Delta u$ .

In 1D,  $Vol_i = 1 \cdot \Delta x_i$  and EUCCLHYD is the Godunov acoustic scheme:

$$u_{i+1/2} = \bar{u}_{i+1/2} - \frac{p_{i+1} - p_i}{2\bar{\alpha}_{i+1/2}} \quad (4)$$

Considering an isentropic flow,  $\frac{dp}{d\rho} = c^2$ :

$$d_t p_i = -(\rho c^2)_i \frac{\bar{u}_{i+1/2} - \bar{u}_{i-1/2}}{\Delta x_i} + \frac{(\rho c^2)_i}{\Delta x_i} \left( \frac{p_{i+1} - p_i}{2\bar{\alpha}_{i+1/2}} - \frac{p_i - p_{i-1}}{2\bar{\alpha}_{i-1/2}} \right) \quad (5)$$

No equivalent term within the “artificial viscosity” framework.

We choose an explicit discretization to describe entropy evolution:

$$m_i T_i^n d_t(s_i) = m_i d_t(e_i) + m_i p_i^n d_t(1/\rho_i) \quad (6)$$

Let us compute it in function of fluxes using equations (1):

$$\begin{aligned} m_i d_t(E_i) &= -[\nabla \cdot (p u)]_i \\ &= m_i d_t(e_i) + m_i d_t(u_i^2/2) \\ &= m_i T_i^n d_t(s_i) - p_i^n [\nabla \cdot u]_i - u_i^n \cdot [\nabla p]_i \end{aligned} \quad (7)$$

**Finally:**  $m_i T_i^n d_t(s_i) = -[\nabla \cdot (p u)]_i + p_i^n [\nabla \cdot u]_i + u_i^n \cdot [\nabla p]_i$

For the EUCCLHYD scheme in 1D, it comes:

$$m_i T_i^n d_t(s_i) = \frac{1}{2} \rho_i c_i \Delta u_i^2 = q [\partial_x u]_i$$

with the equivalent linear artificial viscosity  $q = \frac{1}{2} \rho c \Delta u$ .

Flows with  $u \neq cst$  are computed with an entropy dissipation corresponding to a linear artificial viscosity with coefficient  $1/2$ :

$$m_i d_t(e_i) + m_i p_i^n d_t(1/\rho_i) = m_i T_i^n d_t(s_i) \# \frac{1}{2} \rho_i c_i (\Delta u_i)^2 > 0 \quad (8)$$

Key ideas:

- **We want to reduce EUCCLHYD's entropy dissipation** on isentropic flows.
- **Robustness: same velocity and pressure numerical diffusion** coming from acoustic Godunov solver (no use of Dukowicz solver, A. Burbeau, R. Loubere-P.-H. Maire).
- We allow a trade off with total energy conservation: **quasi-conservation to keep proper shock waves propagation.**

Thus we introduce a parameter  $0 \leq \theta_i \leq 1$  such that:

$$d_t(e_i) + p_i^n d_t(1/\rho_i) = \theta_i T_i^n d_t s_i$$

$$\rightarrow m_i d_t(E_i) = -\theta_i [\nabla \cdot (p u)]_i + (1 - \theta_i) (-u_i^n \cdot [\nabla p]_i - p_i^n [\nabla \cdot u]_i)$$

Rough idea:

When dealing with shock waves:

$\theta_i = 1$ , *EUCCLHYD*, *entropic and total energy conservation*

When computing an isentropic flow:

$\theta_i = 0$ , *isentropic but non conservative in total energy*

*The idea comes from classical schemes with artificial viscosity, and is mentioned in C. Mazeran's PhD thesis 2007 (with B. Després) and D. Chauveheid PhD thesis 2012 (with J.M. Ghidaglia).*

$$R_i = \frac{T_i^n d_t(s_i)}{|p_i^n d_t(1/\rho_i)|} = \frac{-[\nabla \cdot (p u)]_i + u_i^n \cdot [\nabla p]_i + p_i^n [\nabla \cdot u]_i}{|p_i^n [\nabla \cdot u]_i|}$$

The analysis of  $R_i$  (acoustic Riemann problems, strong shock or rarefaction waves) leads to a proposition for  $0 \leq \theta_i \leq 1$ :

$$\underline{T_i^n d_t(s_i) > 0:}$$

$$\rightarrow [\nabla \cdot u]_i < 0 \text{ (shock wave)}$$

$$\theta_i = \min(1, C_q R_i)$$

$$\rightarrow [\nabla \cdot u]_i > 0 \text{ (quasi-conservation of } E_{tot} \text{ and possibly isentropic)}$$

$$\theta_i = \min\left(1, \frac{|p_{i+1}^n - 2 p_i^n + p_{i-1}^n|}{\min(p_{i-1}^n, p_i^n, p_{i+1}^n)}\right)$$

$$\underline{T_i^n d_t(s_i) \leq 0:}$$

$$\theta_i = 1 \text{ (EUCCLHYD scheme).}$$

1D shock wave:  $T_i^n d_t(s_i) \geq 0$ ,  $[\nabla \cdot u]_i < 0$  and  $\theta_i = C_q R_i < 1$ :

$$m_i (d_t(e_i) + p_i^n d_t(1/\rho_i)) = \frac{C_q \left( \frac{1}{2} \rho_i c_i (\Delta u_i)^2 \right)^2}{p_i^n \Delta u_i} \# q_i [\partial_x u]_i \quad (9)$$

It comes a quadratic artificial viscosity:

$$q_i = C_q \left( \frac{\rho_i (c_i)^2}{4 p_i} \right) \rho_i (\Delta u_i)^2 \quad (10)$$

We set  $C_q = 4$  because for perfect gases  $\rho_i (c_i)^2 / p_i = \gamma_i > 1$  should be a proper value as a quadratic artificial viscosity coefficient.

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

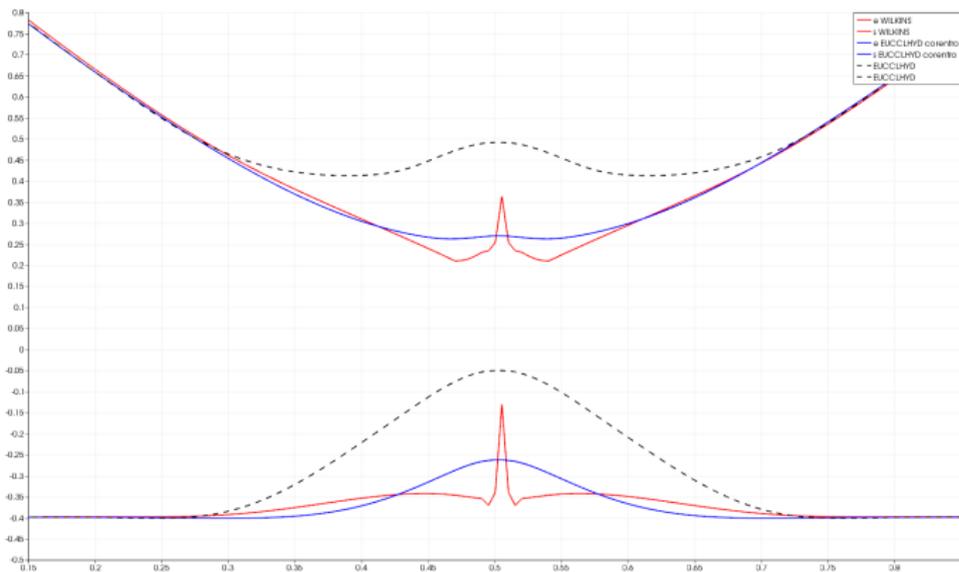


Figure : Double rarefaction wave 1D 200 cells, **internal energy (above), entropy (below)**: EUCCLHYD (black dash), EUCCLHYD quasi-conservation (blue), WILKINS  $Q_{quad}=2$   $Q_{lin}=0.1$  (red).

# Diminishing entropy dissipation EUCCLHYD+Remap

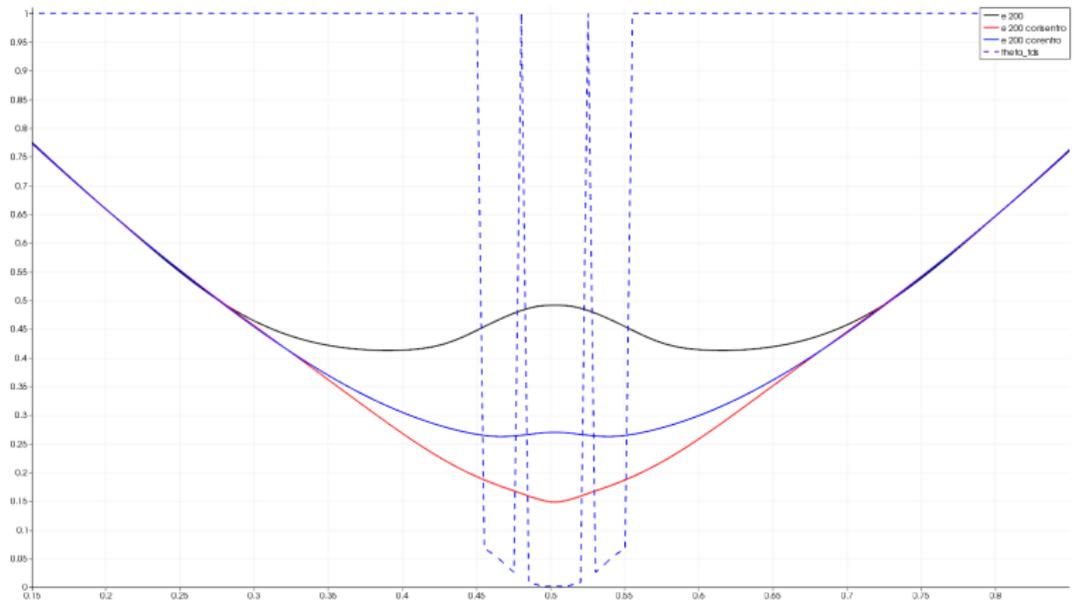


Figure : Double rarefaction wave 1D 200 cells, **internal energy**: EUCCLHYD (black), EUCCLHYD isentropic in rarefaction waves (red) or EUCCLHYD quasi-conservation (blue) with theta (blue dash).

# Diminishing entropy dissipation CONVERGENCE EUCCLHYD + Remap

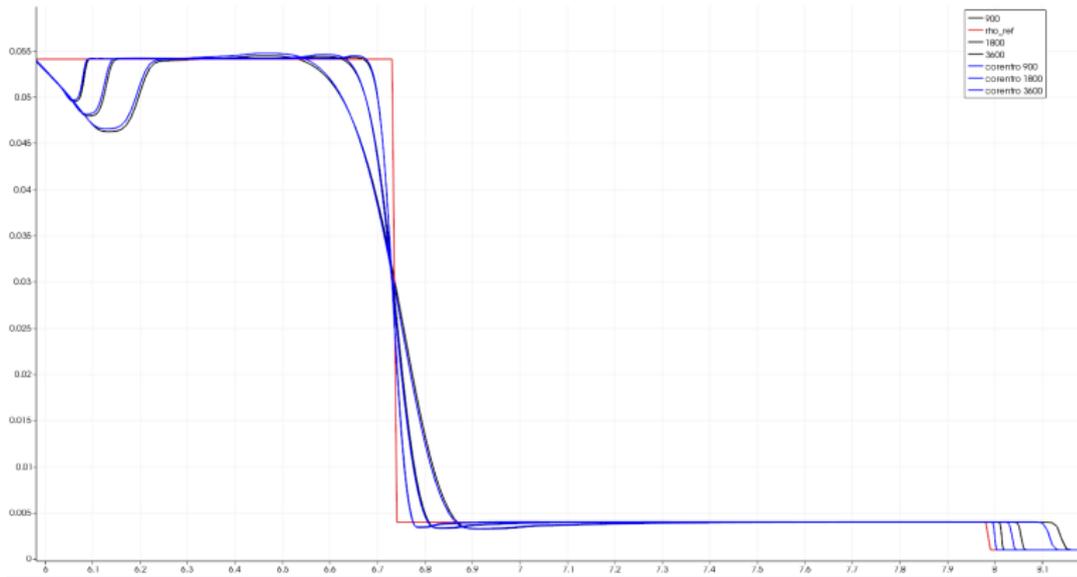


Figure : HELL (LeBlanc Shock tube) 1D 900, 1800 and 3600 cells,  
**density**: EUCCLHYD (black), EUCCLHYD quasi-conservation (blue).

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

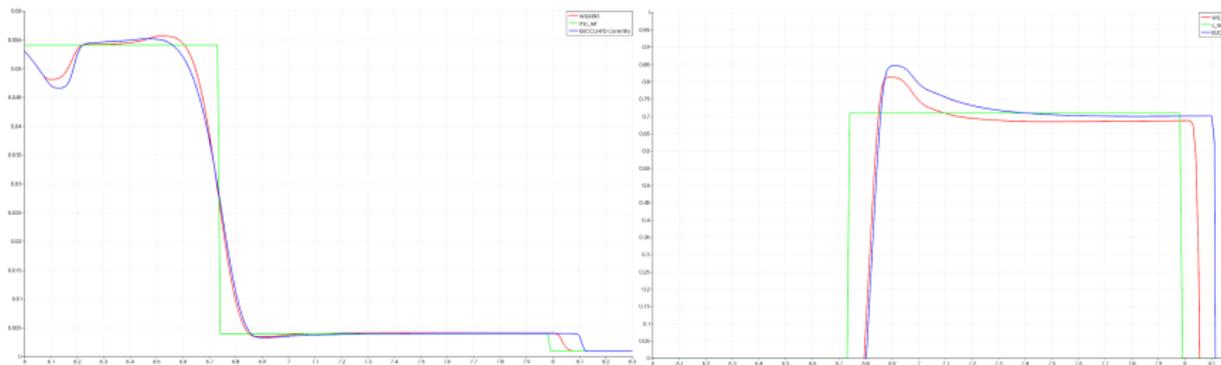


Figure : HELL (LeBlanc Shock tube) 1D 900 cells, **density (left), entropy (right)**: EUCCLHYD quasi-conservation (blue) and WILKINS (red).

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

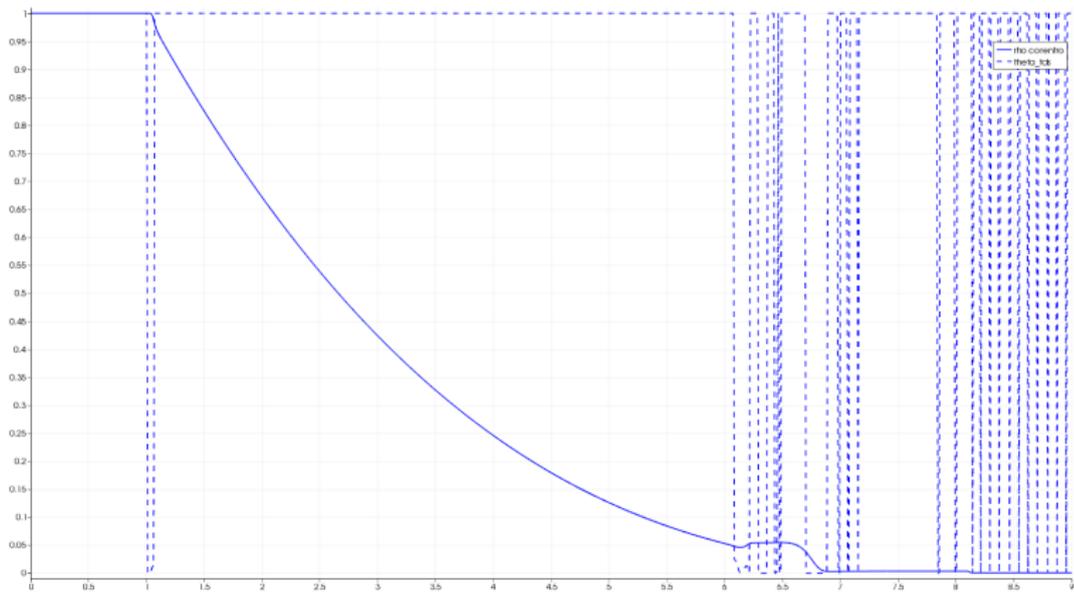


Figure : HELL (LeBlanc Shock tube) 1D 900 cells, **density (blue)** and **theta (blue dash)** for EUCCLHYD quasi-conservation.

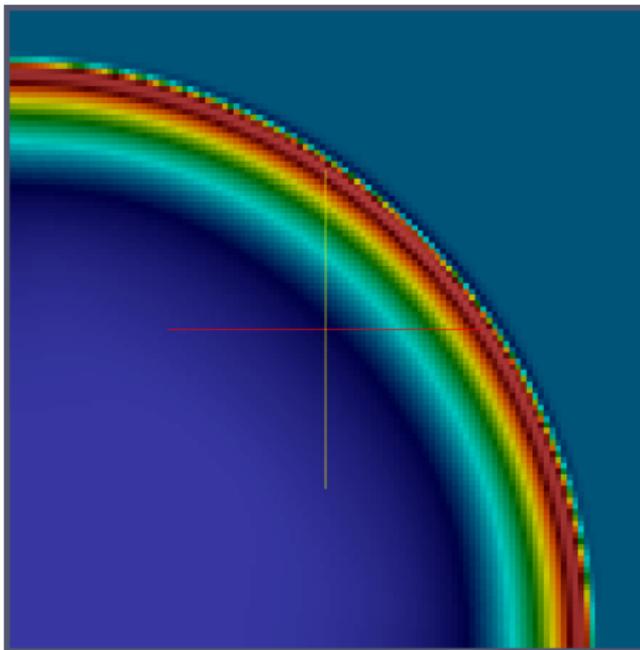


Figure : SEDOV 2D 110x110 cells, **density**.

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

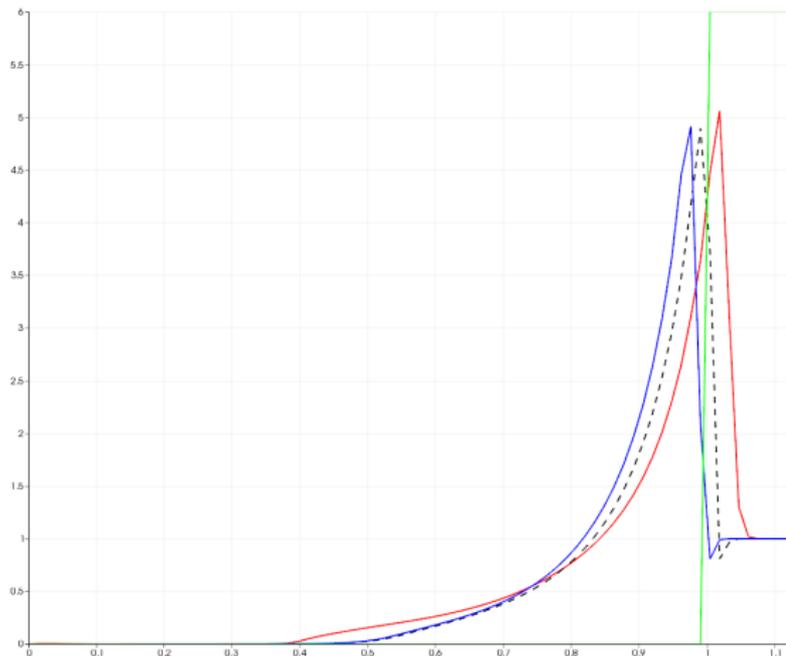
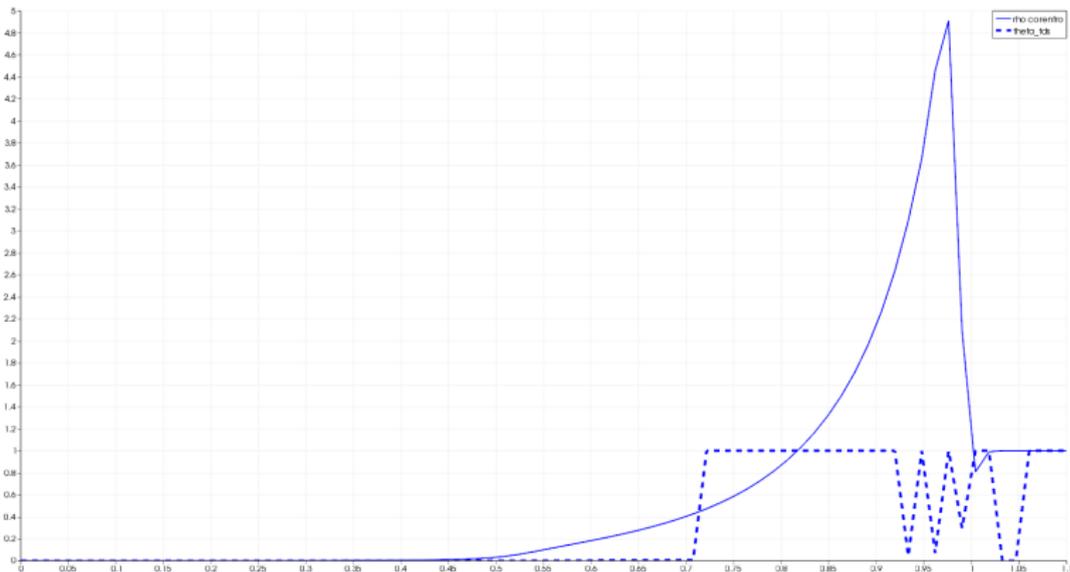


Figure : SEDOV 2D 110x110 cells, **density**: EUCCLHYD (black dash), EUCCLHYD quasi-conservation (blue) or WILKINS (red).

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap



**Figure** : SEDOV 2D 110x110 cells, **density (blue)** with **theta (blue dash)** for EUCCLHYD quasi-conservation.

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

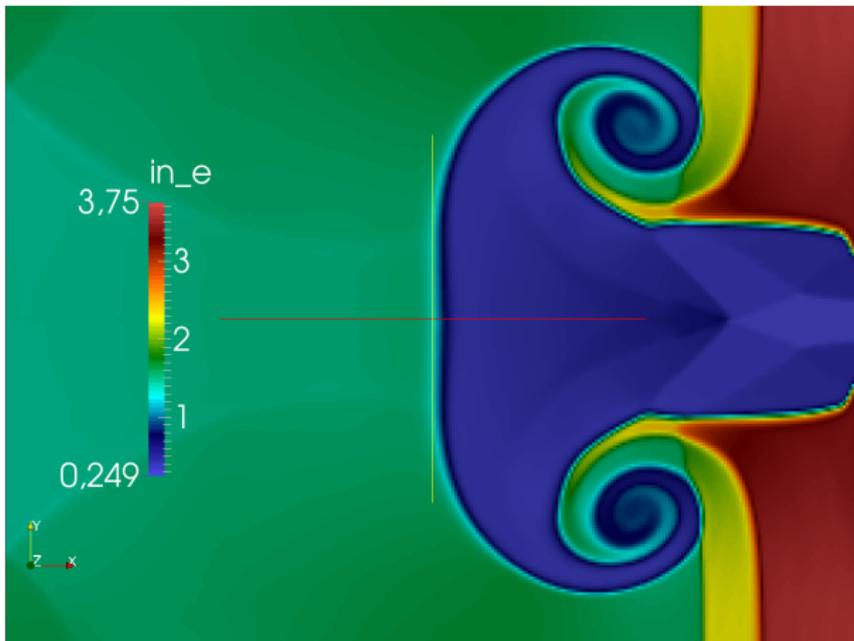


Figure : Triple point 2D 280x120 cells, **internal energy**: EUCCLHYD (top), EUCCLHYD quasi-conservation (bottom).

# Diminishing entropy dissipation WILKINS/EUCCLHYD + Remap

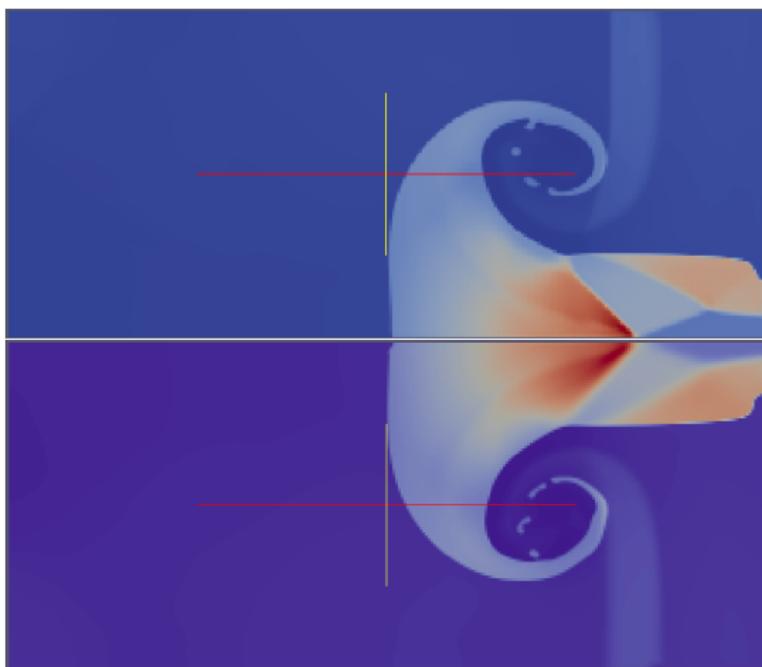


Figure : Multimaterial Triple point 2D 280x120 cells, **density**:  
EUCCLHYD quasi-conservation (top) and WILKINS (bottom).

→ Conservative remap of total energy, effect on internal energy.

Remap phase is achieved by using a flux scheme, thus is fully conservative:

$$\left\{ \begin{array}{l} Vol_i = Vol_i^{lag} + \sum_f dVol_f \\ m_i = m_i^{lag} + \sum_f dm_f \\ u_i = \left( u_i^{lag} m_i^{lag} + \sum_f dq u_f \right) / m_i \\ v_i = \left( v_i^{lag} m_i^{lag} + \sum_f dq v_f \right) / m_i \\ E_i = \left( E_i^{lag} m_i^{lag} + \sum_f dm E_f \right) / m_i \\ e_i = E_i - (u_i)^2/2 + (v_i)^2/2 \end{array} \right.$$

Remap phase is achieved by using a flux scheme, thus is fully conservative:

$$\begin{cases} dm_f & = & \rho_f^{o2} & dVol_f \\ dq u_f & = & \rho_f^{o2} u_f^{o2} & dVol_f \\ dq v_f & = & \rho_f^{o2} v_f^{o2} & dVol_f \\ dm E_f & = & \rho_f^{o2} (e_f^{o2} + k_f^{o2}) & dVol_f \end{cases}$$

$$k_f^{o2} = \frac{(u_f^{o2})^2}{2} - \frac{(u_f^{o2} - u_f^{lag_{upw}})^2}{2} + \frac{(v_f^{o2})^2}{2} - \frac{(v_f^{o2} - v_f^{lag_{upw}})^2}{2}$$

with at face  $f$ :

$\rho_f^{o2}$  the limited linear reconstruction of  $\rho$ ,

$u_f^{lag_{upw}}$  the upwind value on the Lagrange mesh.

Let us consider a **face  $f$  between lagrangian cells  $i$  and  $i + 1$** :

$$m_i E_i - m_i^{lag} E_i^{lag} + dm_f E_f^{o2} = 0$$

$$\rightarrow m_i e_i - m_i^{lag} e_i^{lag} + dm_f e_f^{o2} = \epsilon_i^x + \epsilon_i^y$$

with

$$\epsilon_i^x = m_i^{lag} k_i^{x\ lag} - m_i k_i^x - dm_f k_f^x \ o2$$

$$\epsilon_i^y = m_i^{lag} k_i^{y\ lag} - m_i k_i^y - dm_f k_f^y \ o2$$

with  $k_i^{lag} = (u_i^{lag})^2/2$  and  $k_i = (u_i)^2/2$ .

Since we would like an “adiabatic” remap, we should find  $k_f^x \ o2$  such that  $\epsilon_i^x \approx 0$  and  $\epsilon_{i+1}^x \approx 0$ .

Which value for the kinetic energy flux " $dm_f k_f^{x\ o2}$ " to obtain  $\epsilon_i^x \approx 0$  and  $\epsilon_{i+1}^x \approx 0$  ?

If  $k_f^{x\ o2} = (u_f^{o2})^2/2$ :

$$\rightarrow \begin{cases} \epsilon_i^x = - \left( \frac{dm_f m_i^{lag}}{m_i} \right) \frac{(u_f^{o2} - u_i^{lag})^2}{2} < 0 \\ \epsilon_{i+1}^x = \left( \frac{dm_f m_{i+1}^{lag}}{m_{i+1}} \right) \frac{(u_f^{o2} - u_{i+1}^{lag})^2}{2} > 0 \end{cases}$$

If  $k_f^{x\ o2} = (u_f^{o2})^2/2 - (u_f^{o2} - u_i^{lag})^2/2$ :

$$\rightarrow \begin{cases} \epsilon_i^x = - \left( \frac{(dm_f)^2}{m_i} \right) \frac{(u_f^{o2} - u_i^{lag})^2}{2} < 0 \\ \epsilon_{i+1}^x = \left( \frac{dm_f}{m_{i+1}} \right) \left( m_{i+1}^{lag} \frac{(u_f^{o2} - u_{i+1}^{lag})^2}{2} - m_{i+1} \frac{(u_f^{o2} - u_i^{lag})^2}{2} \right) \end{cases}$$

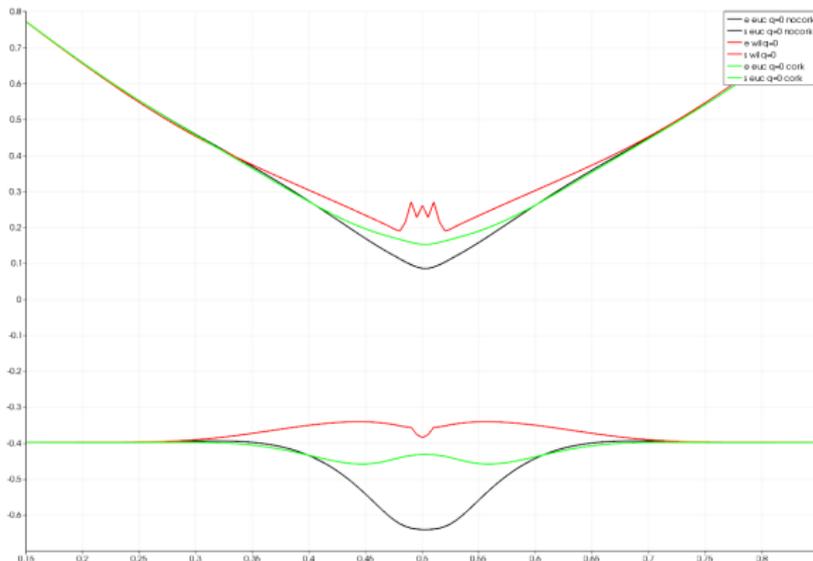


Figure : Double rarefaction wave, 200 cells, **internal energy (above) and entropy (below)**, comparison between isentropic schemes: WILKINS  $q=0$  + internal energy remap, EUCCLHYD  $\theta = 0$  isentropic + total energy remap, with and without corrected “k”.

- Goal: propose a multimaterial scheme adapted to HPC on exascale computers constraints.
- Collocated Lagrange EUCCLHYD-Remap is robust, conservative and entropic (first order).
- Multidirectional direct remap and multimaterial interface sharp reconstruction is classical and robust. An explicit partial pressure relaxation is available.
- The trade off with total energy to reduce entropy error should be further investigated, i.e. quasi-conservation should be proved and quantified.
- The algorithm parallelization efficiency should be evaluated (scalability).