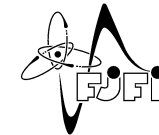


# Symmetry and Volume Compatibility in an r-z Staggered Scheme

**Pavel Váchal**



*Faculty of Nuclear Sciences and Physical Engineering,*  
**Czech Technical University in Prague, Czech Republic**



**Burton Wendroff**

Retired Fellow,

*Theoretical Division,*

**Los Alamos National Laboratory, Los Alamos, USA**



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# Motivation and Purpose

- **Develop a staggered Lagrangian scheme that preserves spherical symmetry while reducing the violation of the Geometric conservation law**

## Outline of This Presentation

- **Introduction**
  - ◇ What do we do and why, staggered grid basics, notation
- **Existing staggered schemes: AW, GC and CV**
- **GCS: The symmetrized scheme**
  - ◇ Boundary conditions
  - ◇ Subcell pressures
- **Numerical results**
  - ◇ Sedov blast wave (sanity checks)
  - ◇ Coggeshall adiabatic compression (convergence study)
- **BONUS:**  
**Wall heating removal by energy exchange à la Noh**

# Introduction: Spherically Symmetric Schemes

- **Why genuinely  $r$ - $z$ , symmetry preserving staggered code?**

- **AW** attractive because it **easily converts any Cartesian scheme** into an axi-symm. one
- Drawback 1: adiabatic flows, no artificial viscosity:  
we would like to have an **accurate approximation to the thermodynamic relation**

$$m_c \frac{d\varepsilon_c}{dt} + \mathcal{P}_c \frac{dV_c}{dt} = 0, \quad \text{which would be true if} \quad \sum_{p(c)} \mathbf{F}_{pc}^p \cdot \mathbf{U}_p = \mathcal{P}_c \frac{dV_c}{dt}$$

This is not the case, in general, for area-weighted, where  $\mathbf{F}_{pc}^p = r_p \mathbf{F}_{pc}^{p,\text{Cart}}$

- Drawback 2: Area-weighted artificial viscosity may in general be **non-dissipative** and may **not conserve  $z$ -momentum**
- In turn, typical existing genuinely  $r$ - $z$  schemes **do not preserve spherical symmetry**

- **Relation to earlier work in staggered discretization:**

- In **[Vachal, Wendroff, JCP 2014]** and **[Vachal, Wendroff, IJNMF 2014]** we **symmetrized artificial viscosity** by a correction of the  $r$ -component of the force
- **Now** we are doing the same **also for pressure forces**

# Staggered Grid Basics

- Nodal dynamics are expressed in the system

$$m_p \left( \mathbf{U}_p^{n+1} - \mathbf{U}_p^n \right) = \sum_{c(p)} \mathcal{P}_c^{n+\frac{1}{2}} \mathbf{G}_{cp}, \quad \mathbf{G}_{cp} = \int_{t^n}^{t^{n+1}} \mathbf{g}_{cp}(t) dt$$

- The nodal motion common to all our methods is

$$\mathbf{X}_p(t) = \mathbf{X}_p^n + \mathbf{U}_p^{n+\frac{1}{2}} (t - t_n), \quad \text{where} \quad \mathbf{U}_p^{n+\frac{1}{2}} = \frac{1}{2} \left( \mathbf{U}_p^{n+1} + \mathbf{U}_p^n \right).$$

- The energy dynamics are expressed as  $m_c \left( \varepsilon_c^{n+1} - \varepsilon_c^n \right) = -\mathcal{P}_c^{n+\frac{1}{2}} \sum_{p(c)} W_{pc}$
- Energy conservation requires that  $W_{pc} = \mathbf{U}_p^{n+\frac{1}{2}} \cdot \mathbf{G}_{cp}$ ,  
while entropy conservation requires that the energy equation be

$$m_c \left( \varepsilon_c^{n+1} - \varepsilon_c^n \right) = -\mathcal{P}_c^{n+\frac{1}{2}} \left( V_c^{n+1} - V_c^n \right).$$

- The *Geometric Conservation Law (GCL)*  $\equiv$  requirement that these expressions are same:

$$\sum_{p(c)} \mathbf{U}_p^{n+\frac{1}{2}} \cdot \mathbf{G}_{cp} = V_c^{n+1} - V_c^n$$

## Existing schemes: AW and GC

- Both assume that the force vector from cell  $c$  on edge  $e$  with endpoints  $p, q$  is

$$\mathbf{f}_{ec} = \mathcal{P}_c \frac{r_p + r_q}{2} \mathbf{n}_{ec}.$$

- Area-weighted (AW)** - see e.g. [Caramana, Burton, Shashkov, Whalen, JCP 1998]

- The contribution to the geometrical force factor is  $\frac{1}{2} r_p \mathbf{n}_{ec} \Rightarrow \mathbf{g}_{cp}^{\text{AW}} = \sum_{e(c,p)} \frac{1}{2} r_p \mathbf{n}_{ec}$ .
- Is symmetric ( $\equiv$  preserves spher. symm. on an equi-angular polar grid)

- Non-symm. GCL Scheme (GC)** - [Loubère, Shashkov, Wendroff, JCP 2008]

- Contribution to geom. force factor  $(\frac{2}{6}r_p + \frac{1}{6}r_q)\mathbf{n}_{ec} \Rightarrow \mathbf{g}_{cp}^{\text{GC}} = \sum_{e(c,p)} (\frac{2}{6}r_p + \frac{1}{6}r_q) \mathbf{n}_{ec}$ .
- Note the factors  $\frac{2}{6}, \frac{1}{6}$ , corresponding to Maire's cell-centered work
- Edge normals  $\mathbf{n}_{ec}$  linear  $\Rightarrow$  integrand in the mom. eq. is a combination of  $rr$  and  $rz \Rightarrow$ 
  - \* These terms quadratic in  $t \Rightarrow \mathbf{G}_{cp} = \int \mathbf{g}_{cp} dt$  can be done exactly with Simpson's rule
  - \* System  $m_p(\mathbf{U}_p^{n+1} - \mathbf{U}_p^n) = \sum_{c(p)} \mathcal{P}_c^{n+1/2} \mathbf{G}_{cp}$  is nonlinear in  $\mathbf{U} \Rightarrow$  iteration required
  - \* The use of Simpson's rule in this way is critical for GCL to be satisfied  
 $\Rightarrow$  **In all calculations below, we perform inner (velocity) and outer (energy) iterations**
- It is well known, that GC is not symmetric.

# Existing schemes: CV

- “Control Volume” (CV)

- Suggested for cylindrical coordinates in [Caramana, Burton, Shashkov, Whalen, JCP 1998]
- Half-edge normals multiplied by  $r$ -coord of their midpoints:

$$\frac{1}{2} \left( r_p + \frac{r_p + r_q}{2} \right) = \left( \frac{3}{4} r_p + \frac{1}{4} r_q \right)$$

⇒ Contribution to geom. force factor is

$$\mathbf{g}_{cp} = \sum_{e(c,p)} \left( \frac{3}{8} r_p + \frac{1}{8} r_q \right) \mathbf{n}_{ec}.$$

- Note that

$$\begin{aligned} \mathbf{g}_{cp}^{\mathbf{CV}} &= \sum_{e(c,p)} \frac{3}{4} \left[ \frac{1}{6} r_p + \left( \frac{2}{6} r_p + \frac{1}{6} r_q \right) \right] \mathbf{n}_{ec} \\ &= \frac{1}{4} \mathbf{g}_{cp}^{\mathbf{AW}} + \frac{3}{4} \mathbf{g}_{cp}^{\mathbf{GC}}. \end{aligned}$$

- Even after Simpson’s integration we get

$$\mathbf{G}_{cp}^{\mathbf{CV}} = \frac{1}{4} \mathbf{G}_{cp}^{\mathbf{AW}} + \frac{3}{4} \mathbf{G}_{cp}^{\mathbf{GC}},$$

⇒ to symmetrize CV we only need to symmetrize GC.

# Symmetry analysis of GC

- Assume fully symmetric data on an equiangular polar grid,

$$\mathbf{X}_{i,j} = (r_{i,j}, z_{i,j}) = (R_j \sin \theta_i, R_j \cos \theta_i),$$

$$\theta_{i+1} - \theta_i = \gamma \text{ for all } i.$$

- Therefore assume also  $m_{i,j} = r_{i,j} A_j$ ,  
where  $A_j$  is indep. of the angle of ray with node  $(i, j)$

- The lack of symmetry in GC lies entirely with the radial component of  $\mathbf{g}$  coming from the edges lying on the same circle, that is, for  $j=\text{constant}$

- Symmetry  $\Rightarrow$  edges on the rays do not contribute to the force (normals opposite, press. equal)
- Consider node  $p = (i, j)$  with circle edges  $(i + \frac{1}{2}, j)$  and  $(i - \frac{1}{2}, j)$
- In order for symmetry to occur, the total geom. factor from these two edges must have the form

$$\mathbf{g}_{i,j}^{\text{circ}} = B_j \sin \theta_i (\sin \theta_i, \cos \theta_i), \quad (1)$$

where  $B$  is independent of angle (= of  $i$ ), because then the contribution to the acceleration is

$$\frac{\mathbf{g}_{i,j}^{\text{circ}}}{m_{i,j}} = \frac{B_j}{R_j A_j} (\sin \theta_i, \cos \theta_i),$$

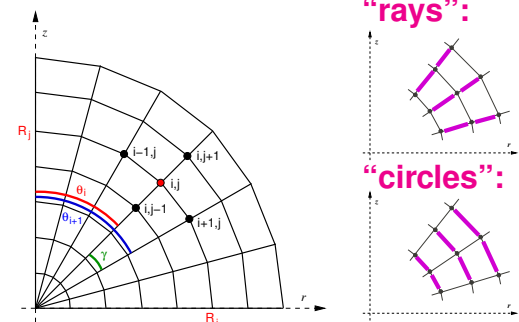
which is spherically radial and has norm independent of angle.

- Now insert for position  $\mathbf{X}$  and normals  $\mathbf{n}$  as in GC, drop const. index  $j$ , and consider the identity

$$\underbrace{(r_{i-1} + 2r_i)(r_i - r_{i-1}) + (r_{i+1} + 2r_i)(r_{i+1} - r_i)}_{\text{6 times the z-component of g from GC}} = \underbrace{(r_{i-1} + r_i + r_{i+1})(r_{i+1} - r_{i-1})}_{=R_j^2 [(2 \cos \gamma + 1) \sin \gamma] 2 \sin \theta_i \cos \theta_i}$$

RHS has the form of the  $z$ -comp. of (1)  $\Rightarrow$  nonsymmetry of GC lies in the  $r$ -component of  $\mathbf{g}$

- This points the way toward symmetrization of GC



# Symmetrization (GCS)

- GC will be **kept as is on the ray edges**.
- On circles, **the  $z$ -component** of the geometrical factor, being already symmetric, **will remain as is**
- **The  $r$ -component will be changed** as required for symmetry, namely

$$g_r = -\frac{1}{6}(r_{i-1} + r_i + r_{i+1})(z_{i+1} - z_{i-1}), \quad \text{which is} \quad \frac{1}{6}R_j^2 [(2 \cos \gamma + 1) \sin \gamma] 2 \sin \theta_i \sin \theta_i$$

by adding a **correction to the  $r$ -comp.** and then accounting for that in the energy equation.

- **In fact, the correction is nothing more than  $g_r$  minus the GC geometric factor, namely,**  

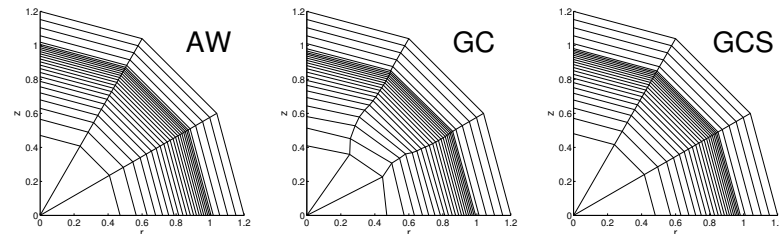
$$\delta = -\frac{1}{6}(r_{i-1} + r_i + r_{i+1})(z_{i+1} - z_{i-1}) + \frac{1}{6}[(r_{i-1} + 2r_i)(z_i - z_{i-1}) + (r_{i+1} + 2r_i)(z_{i+1} - z_i)].$$
- **Notice the identity for this correction  $\delta$ :**

$$12 \delta = (z_{i+1} - 2z_i + z_{i-1})(r_{i+1} - r_{i-1}) - (r_{i+1} - 2r_i + r_{i-1})(z_{i+1} - z_{i-1}).$$

- **In the symmetric case:**

$$\delta = \frac{1}{3} R^2 \sin \gamma (\cos \gamma - 1),$$

- ⇒  $\delta$  is independent of angle
- ⇒ energy change is also symmetric.



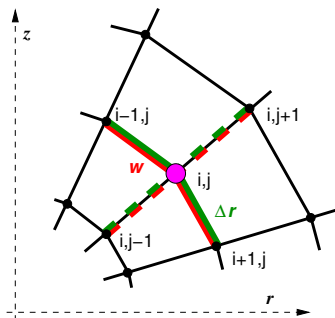
- Of course, **any deviation from GC will not exactly satisfy the GCL**, but (using Taylor expansion for  $\sin \gamma$  and  $\cos \gamma$ ) we see that **the correction  $\delta$  is of 3rd order**, as is the error in entropy.



# The z-axis Boundary Condition

- Assume an equi-angular polar grid with symmetric data (pressure)
  - For an interior node  $(i, j)$ ,  $i > 0$ , the z-component of acceleration in **GC** and **GCS** is

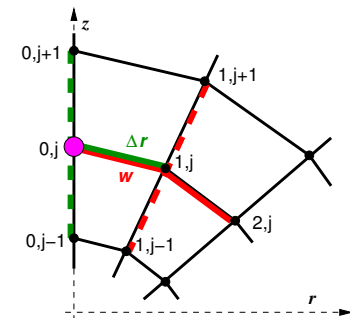
$$\frac{d\delta v_{i,j}}{dt} = \frac{1}{6} \underbrace{\frac{r_{i-1,j} + r_{i,j} + r_{i+1,j}}{m_{i,j}}}_{\text{denote } w, \text{ indep. on } i} \underbrace{(r_{i-1,j} - r_{i+1,j})}_{\text{denote } \Delta r} \left( \mathcal{P}_{j+\frac{1}{2}} - \mathcal{P}_{j-\frac{1}{2}} \right).$$



Stencil of  $\Delta r$  and  $w = \frac{\sum r}{m}$  for the acceleration

← of an interior point  $(i, j)$

of a boundary (z-axis) point  $(0, j)$  →



- On the z-axis ( $i = 0$  ray): We apply reflection  $v_{-1,j} = v_{1,j}$  and use  $\frac{\sum r}{m}$  from the first off-axis node  $(1, j)$ , because it is not defined on the axis (at  $i = 0$ ):

$$\frac{d\delta v_{0,j}}{dt} = \frac{1}{6} \frac{0 + r_{1,j} + r_{2,j}}{m_{1,j}} 2 (-r_{1,j}) \left( \mathcal{P}_{j+\frac{1}{2}} - \mathcal{P}_{j-\frac{1}{2}} \right) = -\frac{1}{3} \frac{r_{1,j} + r_{2,j}}{m_{1,j}} r_{1,j} \left( \mathcal{P}_{j+\frac{1}{2}} - \mathcal{P}_{j-\frac{1}{2}} \right)$$

- Such choice of acceleration of nodes on z-axis also makes sense for a general grid.
- Similarly for the **AW** approach we get

$$\frac{d\delta v_{0,j}}{dt} = -\frac{1}{2} \frac{r_{1,j}}{m_{1,j}} 2 r_{1,j} \left( \mathcal{P}_{j+\frac{1}{2}} - \mathcal{P}_{j-\frac{1}{2}} \right) = -\frac{r_{1,j}^2}{m_{1,j}} \left( \mathcal{P}_{j+\frac{1}{2}} - \mathcal{P}_{j-\frac{1}{2}} \right)$$

# GCS: Subcell pressure forces

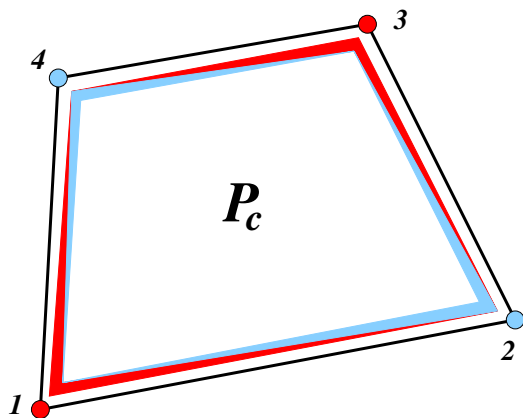
- A technique to **reduce grid distortion**, see [Caramana, Shashkov, JCP 142, 1998]
- **We extend the  $p$ - $c$  notation:**  $s(c)$  are the subcells,  $a(s)$  the nodes of  $s$ , and  $\sum_{s(c)} V_s = V_c$
- These nodes are **averages of the cell nodes**, that is, there is a matrix  $\alpha_{ap}$  such that

$$\mathbf{X}_a = \sum_{p(c)} \alpha_{ap} \mathbf{X}_p \quad \text{with } \alpha_{ap} \geq 0, \quad \sum_{p(c)} \alpha_{ap} = 1.$$

**For example:** for quad cells take quad subcells with  $\mathbf{X}_c = \frac{1}{4} \sum_{p(c)} \mathbf{X}_p$  and  $\mathbf{X}_e = \frac{1}{2}(\mathbf{X}_p + \mathbf{X}_{p'})$ .

- It follows that  $\mathbf{U}_a = \sum_{p(c)} \alpha_{ap} \mathbf{U}_p$ .
- **Each subcell will be treated exactly as the cells are.** That is, we set

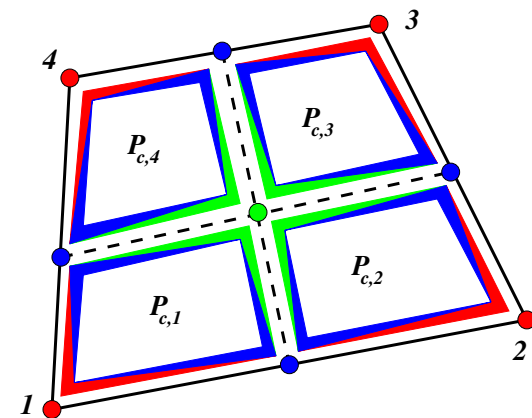
$$\mathbf{G}_{sa} = \frac{\Delta t}{6} \sum_{e(s,a)} \left( (2 r_p^{n+1} + r_{p'}^{n+1}) \left( \frac{2}{6} \mathbf{n}_{es}^{n+1} + \frac{1}{6} \mathbf{n}_{es}^n \right) + (2 r_p^n + r_{p'}^n) \left( \frac{2}{6} \mathbf{n}_{es}^n + \frac{1}{6} \mathbf{n}_{es}^{n+1} \right) \right)$$



Zonal  
pressure  
scheme



Subzonal  
pressure  
scheme



- With subcell pressures  $\mathcal{P}_s$ , the subcell nodal forces are now  $\mathcal{P}_s \mathbf{G}_{sa}$ .

# GCS: Subcell pressure forces

- The cell nodal forces taken to be as in (16)-(17) of [Caramana, Shashkov, JCP 142, 1998],

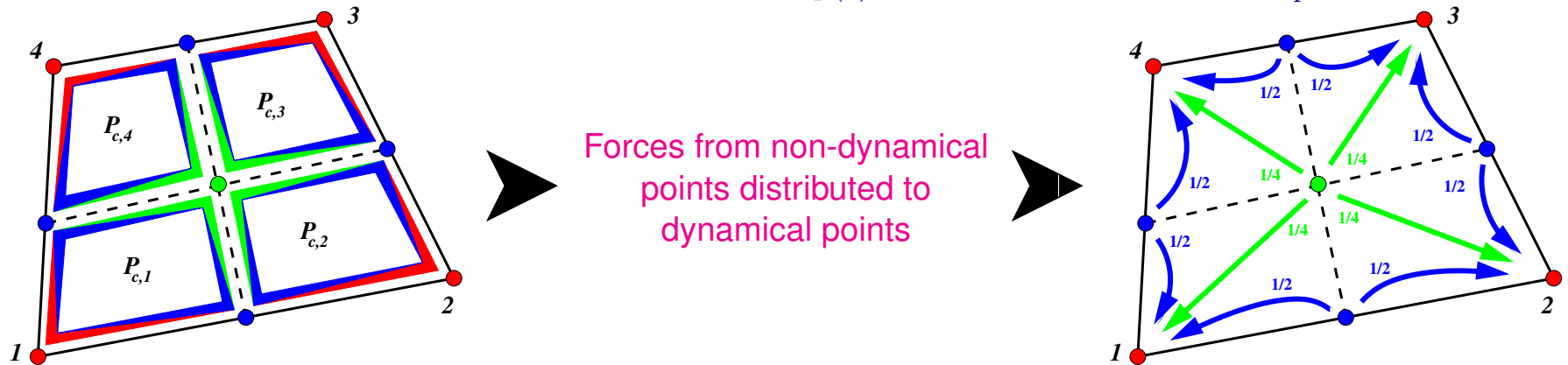
$$\mathbf{F}_{cp} = \sum_a \alpha_{ap} \sum_{s(a)} \mathcal{P}_s \mathbf{G}_{sa}, \quad (1)$$

so that  $m_c (\varepsilon_c^{n+1} - \varepsilon_c^n) = - \sum_{p(c)} \mathbf{U}_p \cdot \sum_a \alpha_{ap} \sum_{s(a)} \mathcal{P}_s \mathbf{G}_{sa} = - \sum_s \mathcal{P}_s (V_s^{n+1} - V_s^n)$ ,

which reduces to  $m_c (\varepsilon_c^{n+1} - \varepsilon_c^n) - \mathcal{P}_c (V_c^{n+1} - V_c^n)$  if the subcell pressures are equal

⇒ **volume compatibility of zonal pressure scheme is “inherited” by the subzonal version**

- Our example with quadrilateral subcells,  $\mathbf{X}_c = \frac{1}{4} \sum_{p(c)} \mathbf{X}_p$  and  $\mathbf{X}_e = \frac{1}{2} (\mathbf{X}_p + \mathbf{X}_{p'})$ :

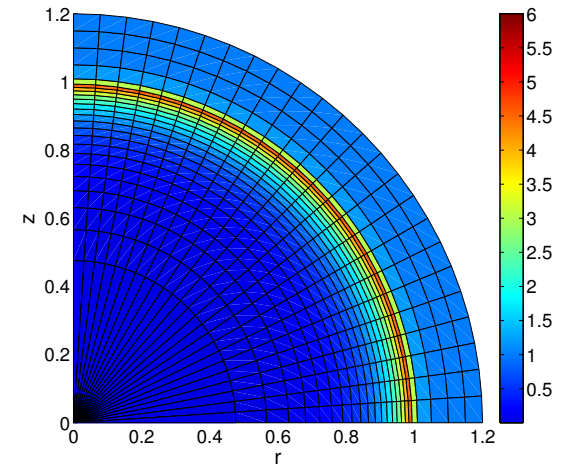
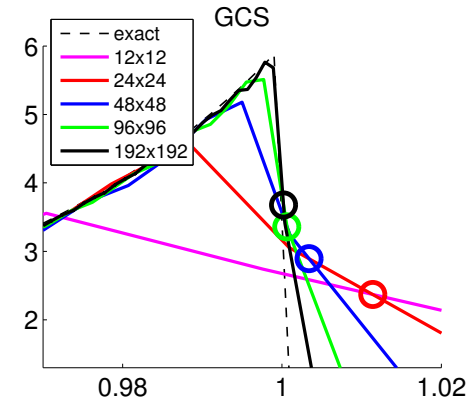
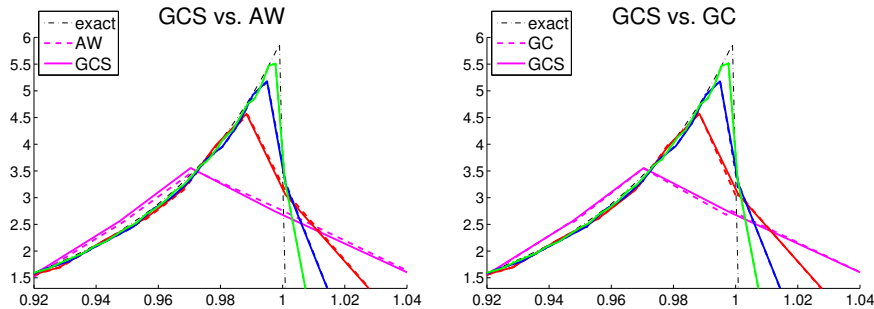
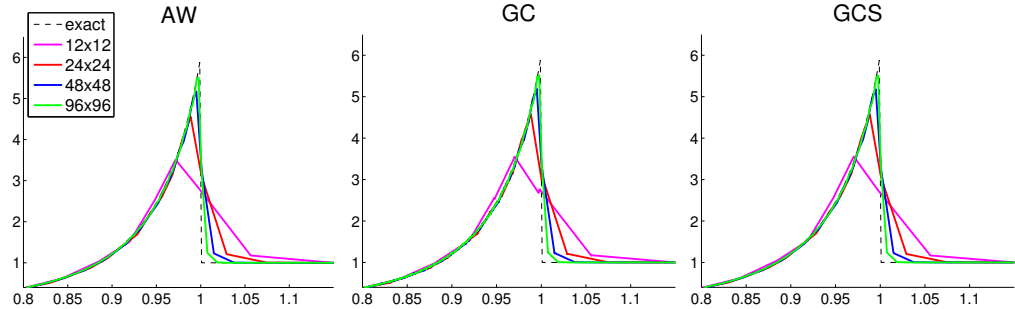


- Other redistribution than (1) and other shapes of subcells are possible
- GCS symmetry corrections**  $\delta_{as}$  calculated per subcell and collected:  $\delta_p = \sum_{s(c)} \sum_{a(s)} \alpha_{ap} \delta_{as}$ .
- AW**: subcells are standard; **CV**: nodal forces combine from AW and GC forces as before

# Numerics: Sedov Test, Zonal Pressure Forces

- Serves as a sanity check that

- the symmetry correction (CG→GCS) does not compromise the shock speed
- AW, GCS and CVS preserve symmetry (unlike GC and CV)



- Viscosity dominates (LapEdge used here)

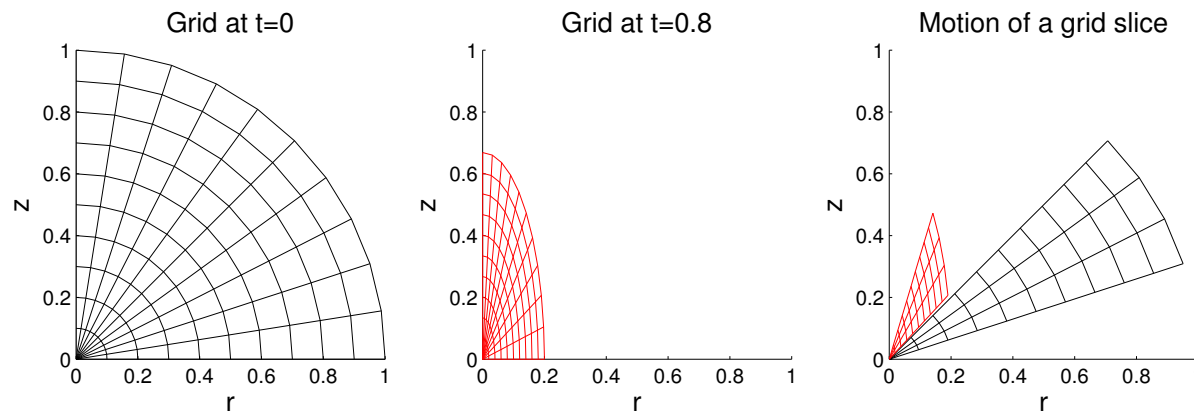
⇒ **most schemes** (press. force types) **perform similarly** (visually same except for small resol.)

# The Coggeshall Test Problem

- A simple adiabatic compression problem that becomes singular at  $t = 1.0$ .
- A sphere of radius 1 is filled with a perfect gas with  $\Gamma = 5/3$  and is collapsing with cylindrical (but not spherical) symmetry so, that the exact solution at a given time  $t$  is

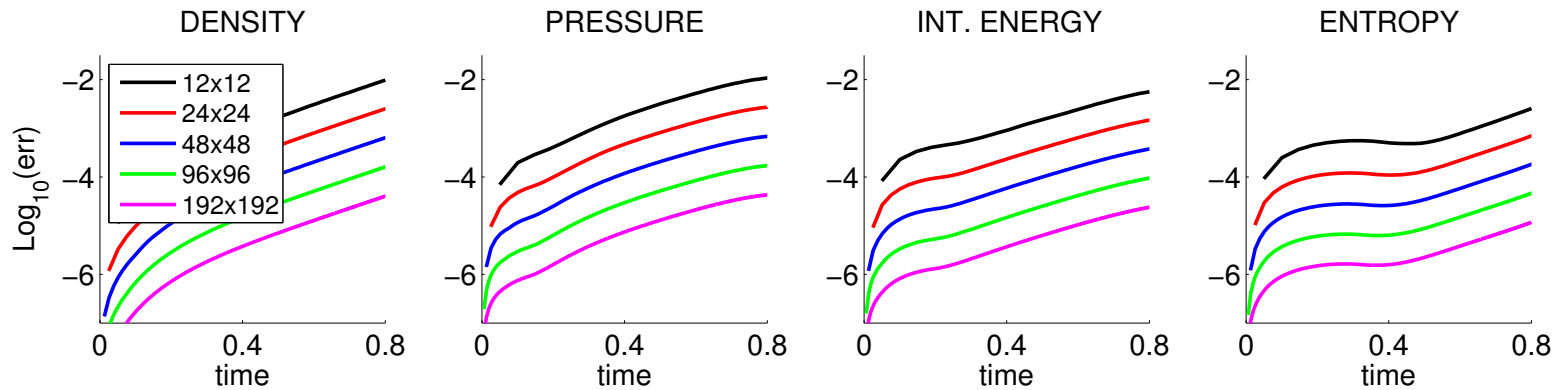
$$u^{\text{ex}}(t) = \frac{-r(t)}{1-t}, \quad v^{\text{ex}}(t) = \frac{-z(t)}{4(1-t)}, \quad \rho^{\text{ex}}(t) = (1-t)^{-9/4}, \quad \varepsilon^{\text{ex}}(t) = \left( \frac{3z(t)}{8(1-t)} \right)^2$$

- Exact BC applied on the outer boundary (spherical outer shell)
- On the  $z$ -axis, all the presented schemes have a simple, problem independent BC
- Entropy is constant on particle paths:  $S^{\text{ex}}(r(t), z(t), t) = S^{\text{ex}}(r(0), z(0), 0)$  at every time  $t$

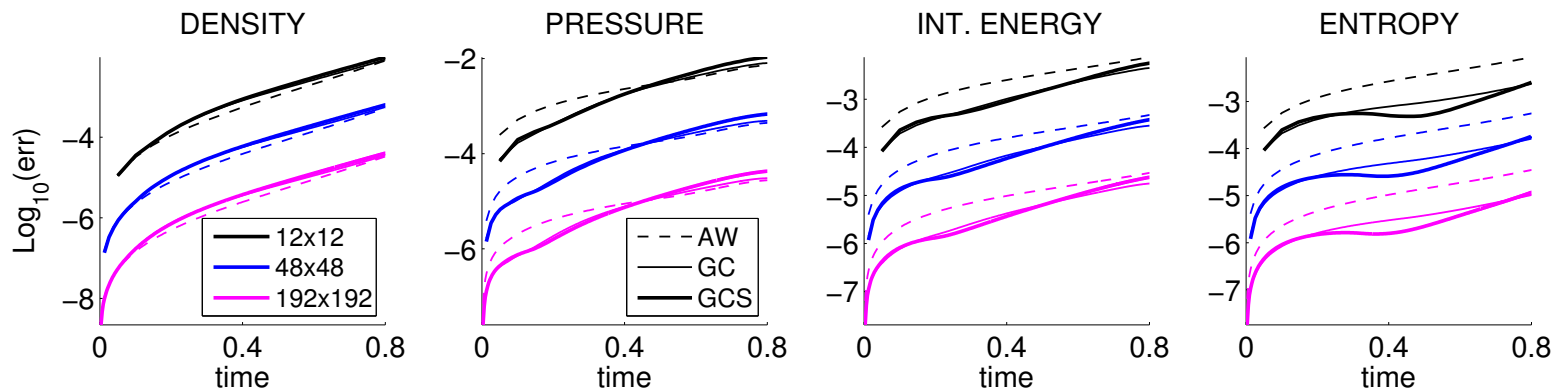


# Numerics: Coggeshall - comparison of AW, GC, GCS

- Evolution of  $\log_{10}$  of  $L_1$  error in time. GCS by thick lines



- Comparison to AW (dashed) and GC (thin solid)

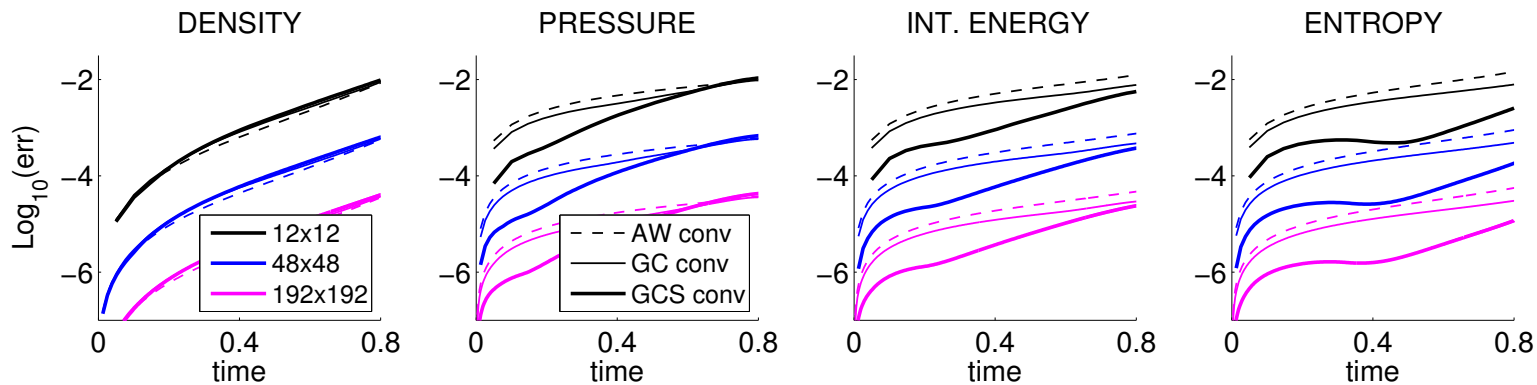


⇒ From the viewpoint of error evolution, GC is superior to AW and GCS similar to GC

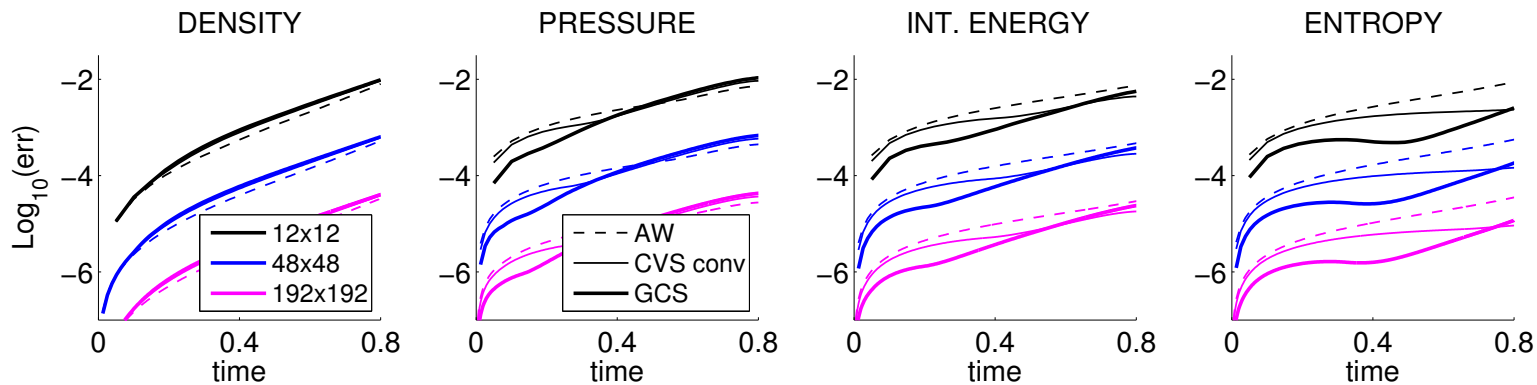
# Numerics: More on Coggeshall

- **NOTE: Outer iterations (predictor-corrector on energy):**

- For our implementation of AW and GC (but not GCS), doing just 2 iterations instead of iterating until convergence gives smaller errors. Previous pictures showed best of each
- In our opinion, **pressure should be iterated until convergence**. Then the comparison is

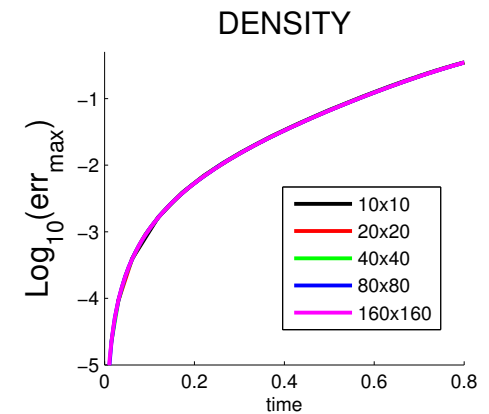
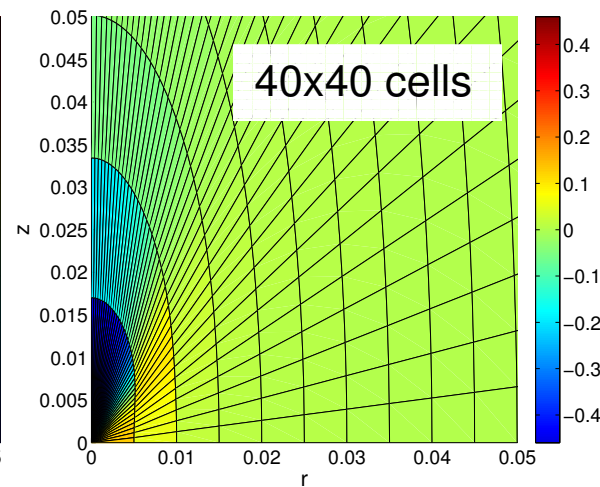
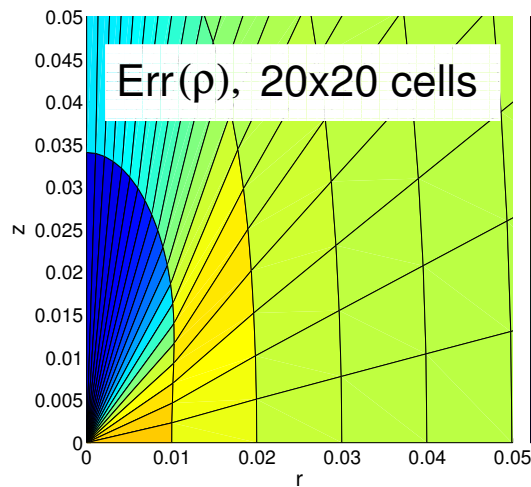


- **Comparison of AW (dashed), CVS (thin solid) and GCS (thick solid)**



# Coggeshall: Remark on the choice of norms

- **Maximum density discrepancy** (particularly in the cell (1, 1) attached to the origin and to the  $z$ -axis) is the same, regardless mesh resolution



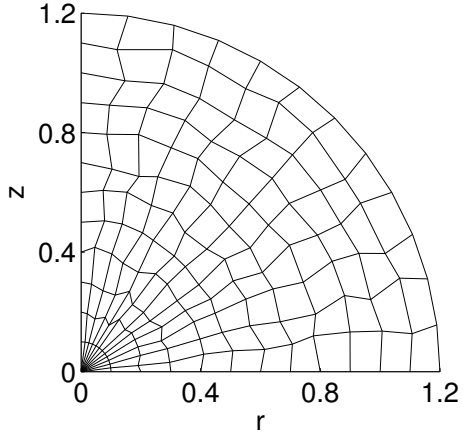
All plots do overlap!

⇒ measuring the density error by the relative  $L_1$  norm  
(and in fact by any norm except for the Maximum norm)  
is a bit misleading

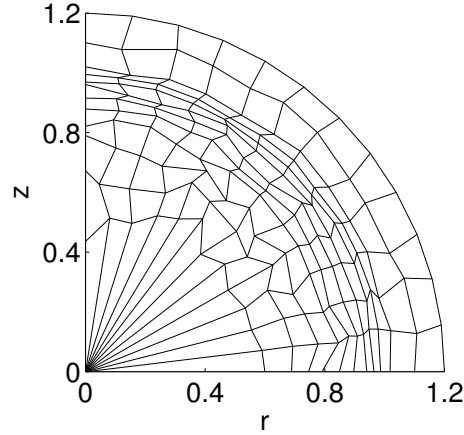


# Numerics: GCS subcells, Sedov on perturbed grid

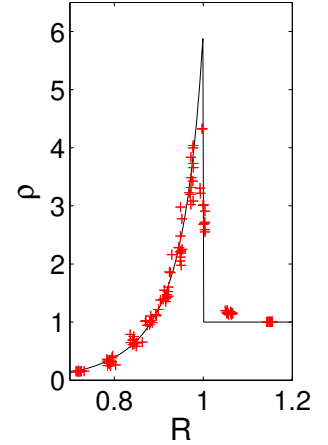
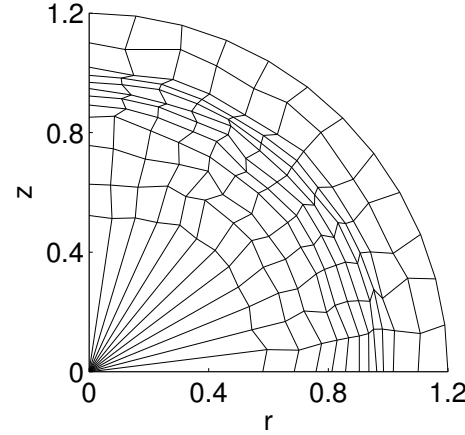
Initial grid ( $t = 0$ )



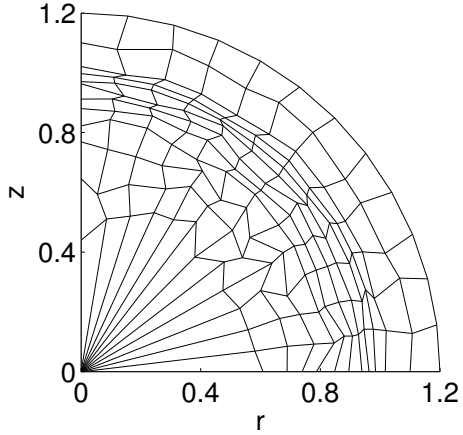
AW,  $M_f = 0$



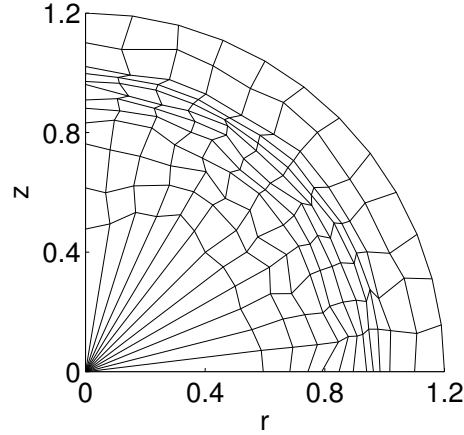
AW,  $M_f = 1$



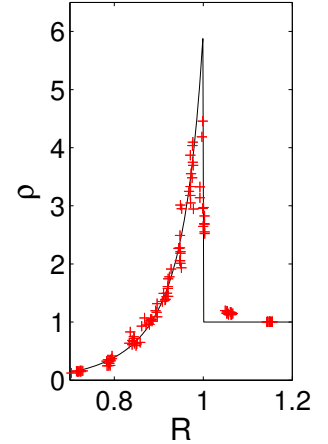
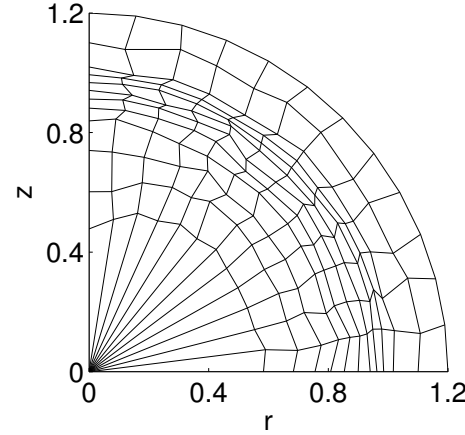
GCS,  $M_f = 0$



GCS,  $M_f = 0.1$



GCS,  $M_f = 1$



# Conclusion

- Developed a **new staggered Lagrangian  $r$ - $z$  scheme GCS** that
  - **conserves total energy**
  - **preserves spherical symmetry for symmetric problems**  
(unlike the existing GC scheme)
  - **keeps the violation of the Geometric Conservation Law small**  
i.e., has more accurate entropy for a particular adiabatic test problem than AW, GC and CV
- **Demonstrated natural incorporation of subcell pressure forces**  
(to prevent / damp unwanted deformations like hourglassing)
- **Performed standard tests to assess the functionality of the scheme**
- **Studied convergence and error evolution in various quantities**  
on the Coggeshall adiabatic compression problem

# BONUS: Wall heating removal by energy exchange

- Tired of seeing wall heating over and over?
- Add a special form of the “heat conduction” as proposed by Noh (**seen anywhere else?**):

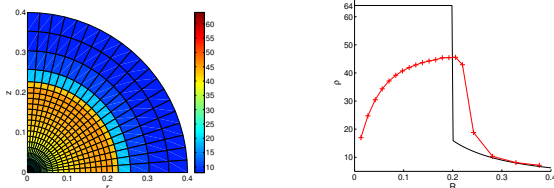
The current energy update  $\varepsilon_c^{n+1} = \varepsilon_c^n + \frac{\Delta t}{m_c} W_c$ , with  $W_c$  being the viscous work,

will be replaced by  $\varepsilon_c^{n+1} = \varepsilon_c^n + \frac{\Delta t}{m_c} (W_c + L_c)$ ,

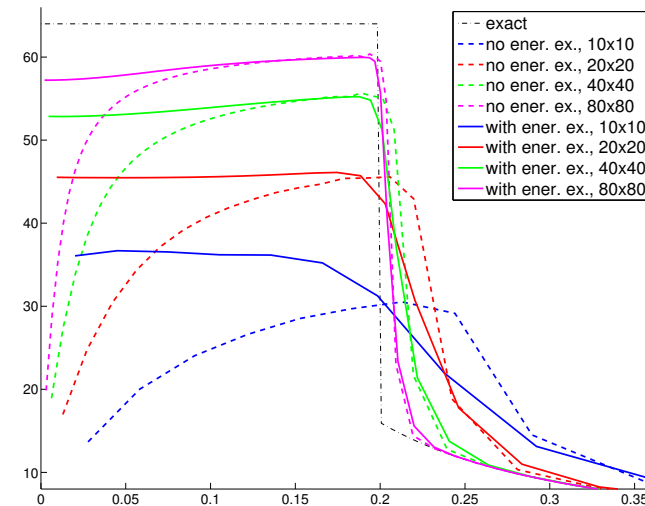
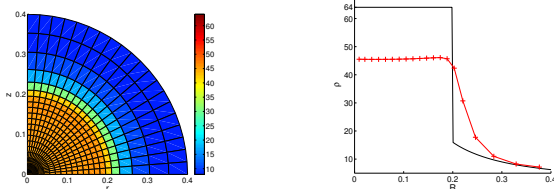
where  $L_c(\varepsilon)$  is a Laplacian type operator on  $\varepsilon$ :  $L_c = \sum_{e(c)} \sigma_e r_e \|\mathbf{l}_e\| (\varepsilon_{c'} - \varepsilon_c)$ .

- Above,  $\|\mathbf{l}_e\|$  is the length of the edge tangent vector (and thus also of the edge), and  $\sigma$  has the dimension of  $\rho$  times  $\mathbf{U}$  (e.g., the average Kuropatenko module of adjac. cells  $c, c'$ )
- **Noh Problem:**

20 × 20 cells, NO ENERGY EXCHANGE



20 × 20 cells, WITH ENERGY EXCHANGE



# Acknowledgments

Many fruitful discussions with  
**Misha Shashkov** on AW schemes  
and **Pierre-Henri Maire** on  $r$ - $z$  schemes  
are highly appreciated

## More Info

- First derivation and description of the GCS scheme in  
**[Proceedings of WCCM XI, ECCM V, ECFD VI, Barcelona 2014]**,  
also available as **[Los Alamos Technical Report LA-UR-14-21791]**
- Full paper including subcell pressure forces  
submitted to **[Journal of Computational Physics]**